

## IMPLEMENTATION OF RESPONSE SURFACE METHODOLOGY USING VARIANCE REDUCTION TECHNIQUES IN SEMICONDUCTOR MANUFACTURING

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### ABSTRACT

Semiconductor manufacturing is generally considered a cyclic industry. As such, individual producers able to react quickly and appropriately to market conditions will have a competitive advantage. Manufacturers who maintain low work in process inventory, ensure that specialized equipment is in good repair, and produce quality products at least possible cost will have the best opportunities to effectively compete and excel in these challenging venues. To support this nimble business model, our current efforts are directed toward creating efficient, accurate metamodels of the impact of maintenance policies on production efficiency. These validated polynomial approximations facilitate rapid exploration of the design region, compared with the original simulation models. The experiment design used for metamodel construction employed variance reduction techniques. When compared to a similar experiment design using independent streams, the variance reduction approach provided a decrease in standard error of the regression coefficients and smaller average error when validated against the simulation response.

## 1 INTRODUCTION

### 1.1 System Description

Semiconductor manufacturing is one of the world's most rapidly developing and growing industries. Manufacturing of semiconductors consists of two consecutive main operations which are called *frontend* and *backend*. The base for most semiconductors today is silicon, which is simply the main element found in sand. Basically, the frontend is the manufacturing of silicon-wafers used to produce the semiconductors. Figure 1 shows a silicon ingot with the slices from it, which will be silicon wafers after patterns are printed and etched on it. After all wafer-level processing is

complete, the wafers are sent to the backend process. The backend operations are comprised of three main facilities: Pre-assembly, assembly, and test/pack operations. After leaving the frontend process, the wafer is thinned in pre-assembly in order to fit in the required package. The back is covered with a thin coating of metal to allow attachment of the wafer to the package. The wafer is then scribed and separated into individual chips. The electrically functioning chips are selected and sent to an assembly operation (Aguilar 2000).



Figure 1: Silicon Ingot and Wafers

This study covers the assembly portion of the backend operations. At the first assembly step, the chip is soldered or glued in the lead frames. Contacts on the dies are then wire-bonded to the leads. The thin gold or aluminum wires are typically 2.5 microns in diameter, and the package may have from eight to several hundred leads. The bonded chips are encapsulated in ceramic or mold compound to hermetically protect the die.

The simulation model used in this study was supplied by one of the world's largest semiconductor manufacturers, Infineon Technologies, originally a part of the Siemens Corporation. The model represents the Malacca Factory, which produces memory products. There are three product families:

- 16M SS8 P-TSOP11-50-1: 0.25 micron process 16 megabit SDRAM

- 64M S20 P-TSOPII-54-1: 0.20 micron process 64 megabit SDRAM
- 256M S20 P-TSOPII-54-1: 0.20 micron process 256 megabit SDRAM

The simulation model contains five different products each of which is a member of one of the above mentioned product families. These five products are distinguished by different processing times and different dedicated tools. These products are:

- Tsop54\_ss4\_x4
- Tsop54\_ss4\_x8
- Tsop54\_ss4\_x16
- Tsop54\_256M
- Tsop54\_S19\_x8

In the assembly area all five products follow the same process flow. The process flow chart of the assembly operations is provided in Figure 2. The flow contains ten main steps: *die bonding*, *wire bonding*, *prebake*, *molding*, *post mold cure*, *dedam/dejunk*, *plating*, *trim and form*, *PC by off*, and *packing*.

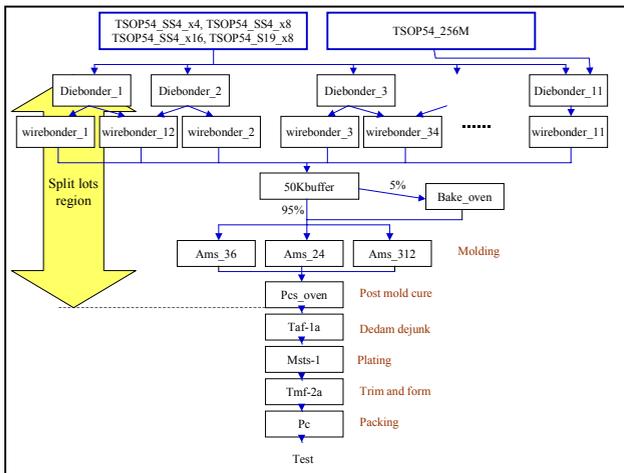


Figure 2: Process Flow Diagram

As seen in the flow chart of Figure 2, there are 11 parallel lines, each of which has a diebonder and a number of wirebonders. These lines are called *autolines*, and the configuration is depicted in Figure 3. The configuration depends on the number of the diebonders and the wirebonders. One autoline can have up to two diebonders and 10 wirebonders. As shown in Figure 3, some of the autolines share one wirebonder. The initially formed product lots are split into magazines before going into the autolines and combined after the post mold cure operation. The default magazine size is 480 units for all of the products (Potoradi 2000).

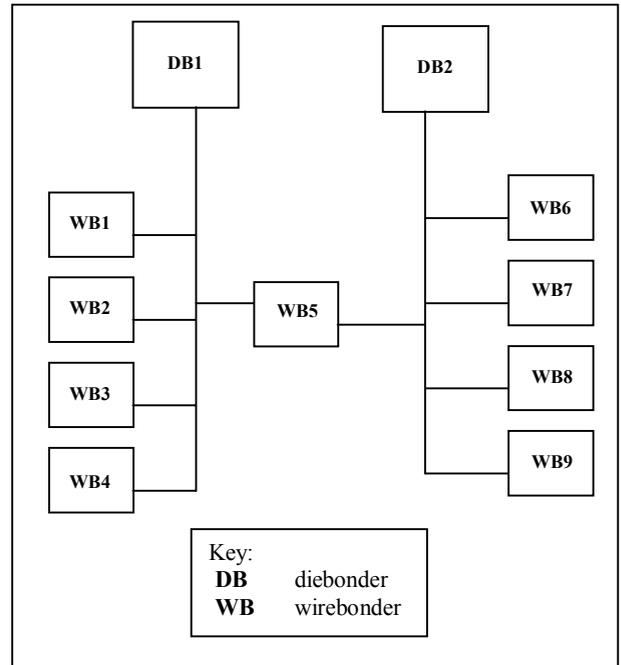


Figure 3: Autoline Configuration

## 1.2 Measures of Performance and Key Variables

### 1.2.1 Model 1

Initial analysis efforts revealed that the processing time of the molding machines and the time between releases were significant determinants of system performance. We used both to predict work in process (WIP).

### 1.2.2 Model 2

To optimize Model 1, one would minimize WIP by maximizing the time between releases and minimizing the processing time. Due to the practical limitations of Model 1, we also considered a cost model. The decision variables in this model were the time between, and duration of, both scheduled and unscheduled maintenance. These variables have an effect on both WIP and Cycle Time, which are performance measures used to calculate cost per part in the objective function.

## 1.3 Optimization

When the objective to be optimized depends on a complex model, one can use Response Surface Methodology (RSM) (Neddermeijer et al. 2000; Myers and Montgomery 1995; Barton 2000). The steps of RSM are presented in Figure 4. At the core of this process is the fitting of a full quadratic model and is the focus of our study.

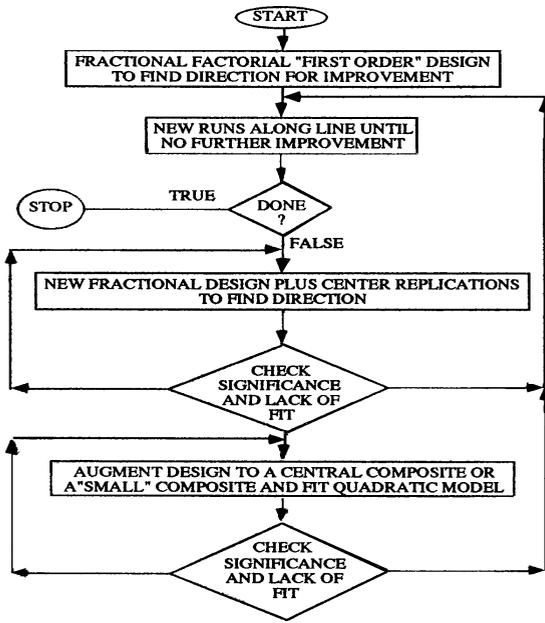


Figure 4: Response Surface Methodology

### 1.4 Purpose of the Paper

This paper shows the application of RSM technology to a backend assembly maintenance decision. A variance reduction technique was employed to observe its impact on the precision of the metamodels. Towards this end, we present the implementation of RSM using variance reduction in Section 2. The results of this approach are outlined in Section 3, while recommendations are presented in Section 4.

## 2 RESPONSE SURFACE MODELS

### 2.1 Variance Reduction Techniques

Using antithetic variates to reduce the variance of a single system, we seek to induce negative correlation between separate simulation runs. In this way, a small observation in one run is offset by a large observation in the complementary run. Taking the average of the pair, it will tend to be closer to the common expectation  $m$  of an observation than if the two observations were generated independently (Law and Kelton 2000).

We observe a pair of responses  $Y^{-1}$  and  $Y^{-2}$  where  $Y^{-2}$  is the obtained from the properly synchronized antithetic run corresponding to  $Y^{-1}$ . We take the average of these two responses as the estimate of the true performance mean. Then,

$$Var\left(\frac{Y^{-1} + Y^{-2}}{2}\right) = \frac{Var(Y^{-1}) + Var(Y^{-2}) + 2Cov(Y^{-1}, Y^{-2})}{4} \quad (1)$$

Hence, we seek negative correlation between  $Y^{-1}$  and  $Y^{-2}$  to reduce the variance. (Schmeiser 1999). To induce this correlation structure, we use complementary random numbers. If random number  $U$  is used for a particular purpose in the model, we use  $1-U$  for this same purpose in the second run.

The use of common random numbers is restricted to comparisons of two or more alternative system configurations. Considering responses  $Y_1$  and  $Y_2$  from two configurations,

$$Var(Y_1 - Y_2) = Var(Y_1) + Var(Y_2) - 2Cov(Y_1, Y_2) \quad (2)$$

If the simulations are conducted with different random numbers, the two configurations will be independent. Hence,  $Cov(Y_1, Y_2) = 0$ . However, if we can induce a positive correlation between  $Y_1$  and  $Y_2$ , then  $Cov(Y_1, Y_2) > 0$ , and we will have reduced the variance of  $(Y_1 - Y_2)$  in Equation (2) compared to the independent configurations.

Hence, we seek positive correlation between  $Y_1$  and  $Y_2$  to reduce the variance. We attempt to induce this correlation by using the same random numbers to simulate each configuration. Further, these random numbers must be synchronized for use in the same purpose within every configuration. Law and Kelton (2000, pp. 586) summarize, “Ideally, a specific random number used for a specific purpose in one configuration is used for exactly the same purpose in all other configurations.”

For example, if a particular random number is used to generate the arrival time of a lot of chips to backend assembly, then it should be used in future configurations to generate the same arrival time rather than for the generation of a processing time or other purpose. If we cannot ensure this synchronization, the full benefit of CRN will be lost. Despite concerted effort, it is possible that a CRN implementation will lead to an increase in variance of  $(Y_1 - Y_2)$  by causing negative correlation. Therefore, validation is required.

### 2.2 Factory Explorer Implementation

Antithetic variate implementation in *Factory Explorer* was accomplished with a beta version of the software. It contains a run option that allows the user to specify antithetic random numbers for a given starting stream.

Using a common random number scheme in *Factory Explorer* involved assigning a separate random number stream to each source of variation in the backend assembly model. By dedicating streams to specific purposes, we have a much better chance of using the same random numbers for the same purpose as the system configuration is altered.

As explained by the *Factory Explorer* documentation (1995), the synchronization of the random number streams gradually degrades with multiple replications. The rec-

ommended remedy is to specify an arbitrary stream offset. Suppose we choose an offset of 500 and consider any one random number stream. Then, when the first replication is complete, the stream would effectively be “rewound” to begin at the 500th random number obtained in the first replication. The documentation describes this as resetting the synchronization. We implemented this offset refinement to CRN in our models with an arbitrary value of 100.

**2.3 Use of the Schruben-Margolin Design**

The Schruben-Margolin experimental design as shown in Figure 5 is based on a central composite design (Schruben and Margolin 1978).

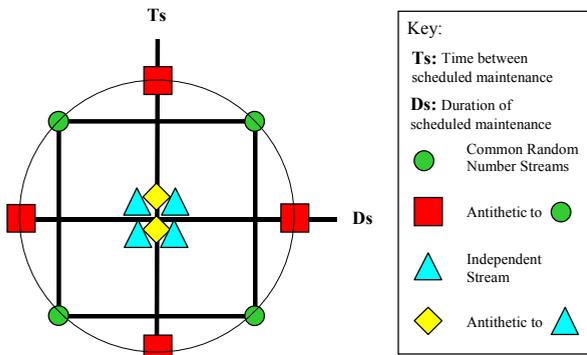


Figure 5: Schruben-Margolin Graphical Design

It incorporates variance reduction techniques in the following manner. Corner points are run using a common random number strategy. Axes points are antithetic runs corresponding to the corner points. Typically, there are antithetic and independent runs made at the center to aid the estimation of lack of fit.

Compared to the use of common random numbers for all points, the Schruben-Margolin approach reduces the bias of the fitted model coefficients. Compared to a corresponding design made only with independent streams, the Schruben-Margolin design results in decreased standard errors of the fitted model coefficients (Schruben and Margolin 1978).

A rotatable central composite design formed the basis of our particular Schruben-Margolin implementation. Thus, axes and corner points were equidistant from the center of the design. Geometrically, this distance was  $\sqrt{2} \cdot \text{design range} / 2$ . Four independent runs were made at the center with two additional antithetic replications corresponding to two of the independent runs.

**2.4 Key Factors and Objectives**

Derivation of the objective function is summarized by Table 1. A cost model was developed to capture the effect of model changes on the cost per part, Equation (5). This per

part cost is a summation of the components of production cost divided by the total production volume in a unit period. The four terms in this cost function are: manufacturing cost, inventory cost, unscheduled maintenance cost, and scheduled maintenance cost. Manufacturing cost,  $Mc$ , as defined above is the manufacturing cost per day of the backend assembly. The total inventory cost is calculated by a product of the per part daily inventory holding cost and average daily work in process for a given run length. Unscheduled and scheduled maintenance costs are determined in a similar manner; labor rates are multiplied by the total required maintenance time. There is a perceived inverse relationship between the amount of scheduled maintenance and the subsequent occurrences of unscheduled maintenance required. This is captured through Equations (3) and (4) where, as the time between scheduled maintenance increases over the nominal time, the frequency and duration ( $1/T_u$  and  $D_u$ , respectively) of unscheduled maintenance will increase.

Table 1: Cost Model Components

Quantity	Units
$C_p$ : Cost/part	\$/part
$D_u$ : Duration of unscheduled maintenance	days
$D_s$ : Duration of scheduled maintenance	days
$D_{s_0}$ : Initial duration of scheduled maintenance	days
$T_u$ : Time between unscheduled maintenance	days
$T_s$ : Time between scheduled maintenance	days
$T_{s_0}$ : Initial time between scheduled maintenance	days
$T^T_u$ : Total unscheduled maintenance time	days
$T^T_s$ : Total scheduled maintenance time	days
$M_u$ : Unscheduled maintenance cost rate	\$100/hour
$M_s$ : Scheduled maintenance cost rate	\$100/hour
$I_c$ : Inventory holding cost	\$/part/day
$CT$ : Cycle Time	hours/part
$WIP$ : Work in Process	parts/day
$TP$ : Throughput	parts/day
$Mc$ : Manufacturing cost of back-end factory	\$150,000/day
$RL$ : Simulation run length	days

$$T^T_s = RL(D_s/T_s)$$

$$T^T_u = RL(D_u/T_u)$$

$$T_u = T_{u_0} + (T_{s_0} - T_s) + (D_s - D_{s_0}) \tag{3}$$

$$D_u = D_{u_0} + .01(T_s - T_{s_0}) + (D_{s_0} - D_s) \tag{4}$$

$$C_p = (Mc + I_c * WIP * RL + M_u * T^T_u + M_s * T^T_s) / (TP * RL) \tag{5}$$

**2.5 Experiment Designs and Implementation**

A summary of the experimental approach is depicted by Figure 6. For a Schruben-Margolin design on time between scheduled maintenance ( $T_s$ ) and duration of scheduled maintenance ( $D_s$ ), the simulation runs were made to observe the corresponding factory performance characteristics. We used the resulting data to calculate the cost per

part according to the cost model and fit a polynomial metamodel for use with Response Surface Methodology.

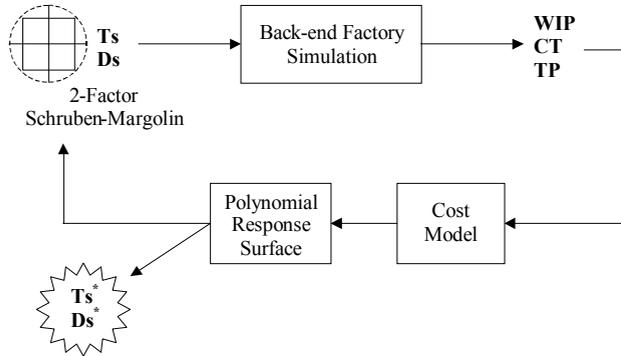


Figure 6: Experimental Procedure

### 3 RESULTS

The Schruben-Margolin design was used in the analysis for two reasons. First, we wanted to explore the ramifications of using a design strategy based on variance reduction techniques in Response Surface Methodology. Secondly, this design, in theory, reduces the error in the regression models. To validate this premise a study was conducted to compare the Schruben-Margolin design with a design that only used independent random number streams. The validation was conducted for both models used in this study, time between releases (TBR) and processing time of the bottleneck molding machines (PTM) as determinants of WIP, and time between scheduled maintenance (Ts) and duration of scheduled maintenance (Ds) as predictors of cost.

The same central composite design that was used in the first iteration of each optimization was run using only independent random number streams. Then, a first order regression model was fit for Model 1, and a full quadratic was fit for Model 2. Standard errors were computed for the coefficients of the regression model created using the Schruben-Margolin design and the independent stream design. The results provided in Tables 2 and 3 show the standard error is less for the coefficients generated by the Schruben-Margolin design for both models. We conclude that the use of Schruben-Margolin design provides a model with less error and therefore, creates a more accurate model.

Figure 7 presents a graphical representation of one of the response surfaces generated through RSM using a full quadratic model of time between and duration of scheduled maintenance to predict the cost per part. As depicted, the normalized search direction to minimize the unit cost is (+1, +1).

Table 2: Schruben-Margolin vs. Independent Stream Designs for Model 1

Coefficient	Standard Error	
	Independent	Schruben-Margolin
INT	9321	8832
PTM	14181	13437
TBR	14181	13437

Table 3: Schruben-Margolin vs. Independent Stream Designs for Model 2

Coefficient	Standard Error	
	Independent	Schruben-Margolin
INT	6.306	3.000
Ts	8.526	4.056
Ds	8.526	4.056
Ts*D <sub>s</sub>	5.265	2.505
Ts*Ts	3.932	1.871
D <sub>s</sub> *D <sub>s</sub>	3.932	1.871

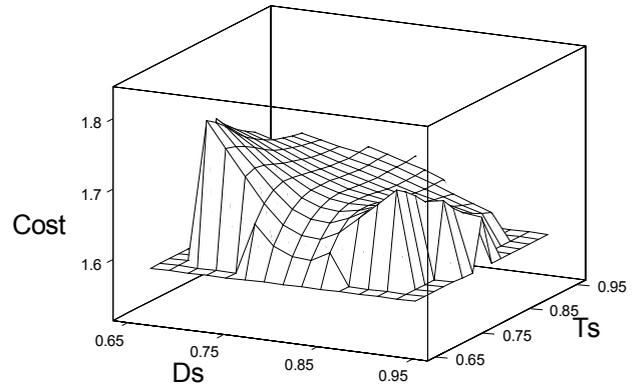


Figure 7: Predicted Response of Cost vs. Duration and Time Between Scheduled Maintenance for a Quadratic Model Fit During RSM Implementation

### 4 RECOMMENDATIONS

With respect to the semiconductor manufacturer, it appears that a reduction in time between and duration of scheduled maintenance could yield a reduction in cost per part. From the results of the RSM implementation, a 10-15% reduction would be appropriate.

Metamodeling efforts using the variance reduction techniques led to a decrease in standard errors of the fitted regression model coefficients compared to a similar design implemented with independent replications. Further, the Schruben-Margolin design had lower average absolute error when validated against the simulation response. In closure, it would be advisable to use common random numbers and antithetic variates in RSM.

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